GEOTECHNICAL PRESENTATION TO THE NATIONAL ACADEMY OF SCIENCES NIAGARA FALLS STORAGE SITE SUBCOMMITTEE

JUNE 29-30, 1994

Graphic Index with Sources

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| 10 | | Regional Bedrock from the Allegheny Plateau | , , , , , |
| | | to the Laurentian Plateau, South to North. | NFSS Geologic Report, 1984 |
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| | | Zones of the Fractured Shale/Glacial Till, and | Services, Inc. Townships of Porter and |
| | | Alluvial Materials on August 24, 1977 | Lewiston, New York, 1977 |
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| 31 | | Monitoring Well Locations around Waste | DOE NEGO A 40 T - 1' 1000 |
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| | | Profile from the NFSS WCS to Modern Municipal | |
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CONSIDERATIONS FOR LONG-TERM STORAGE OF RADIOACTIVE MATERIALS

- Structural stability
- Relationship of the facility to the 100-year floodplain
- Composition of the underlying materials
- Design of the facility
- Risk to drinking water aquifers

STRUCTURAL CONSIDERATIONS

- Proximity to known and active faults
 - No active faults in proximity to NFSS
- Karst formation (caverns)
 - No limestone units in proximity to NFSS
- Stability of soils underlying the facility
 - Underlying soils are stable under the design load conditions

SURFACE WATER CONSIDERATIONS

- The facility should not be located in a 100-year floodplain
 - NFSS is not in a 100-year floodplain
- The facility should not pose a threat to a wetland in the event of a release
 - NFSS is not located in a wetland and does not pose a threat to wetlands

COMPOSITION OF UNDERLYING MATERIALS

- Geological materials underlying the facility should have the capacity to retard the movement of contaminants in the event of a release
- Predominantly unconsolidated clay units to bedrock
- Bedrock composed of shale
- Absence of limestone units in the area

DESIGN CONSIDERATIONS

- Contains and confines the waste
- Structurally stable
- Prevents inadvertent intrusion
- Inhibits migration of the waste
- Reduces surface water infiltration

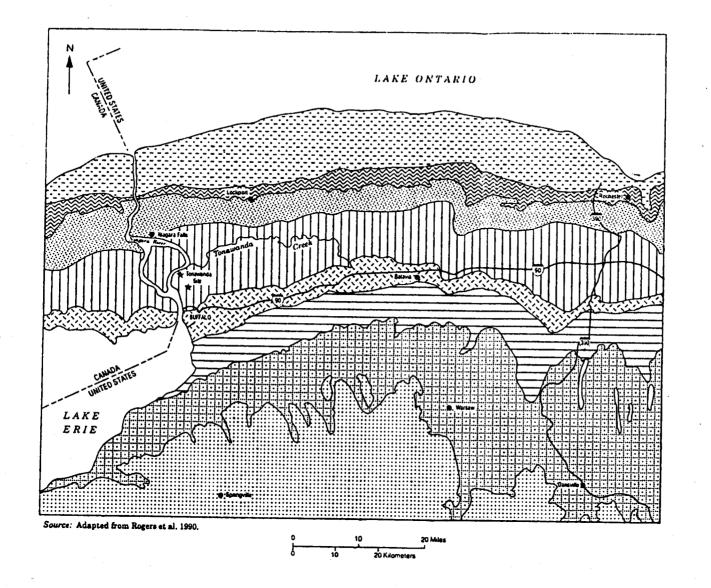
NFSS has a modified UMTRA cap design that achieves each of the listed objectives

GROUNDWATER CONSIDERATIONS

- The facility should not pose a threat to the local drinking water aquifers
 - No local drinking water aquifers underlay NFSS

REGIONAL GEOLOGIC STRUCTURE AND STRATIGRAPHY

- Bedrock dips to the south-southeast
- Clarendon-Linden structure
- Seismically stable
- Bedrock composed of Queenston shale
- Bedrock covered by a layer of unconsolidated materials composed primarily of lake clays



EXPLANATION

DEVONIAN

Canadaway Group

West Falls, Sonyea, and Genesce Groups and Tally Limited

Ham

Hamilton Group



Onondaga Formation

SILURIAN



Salina Group



Lockport Group



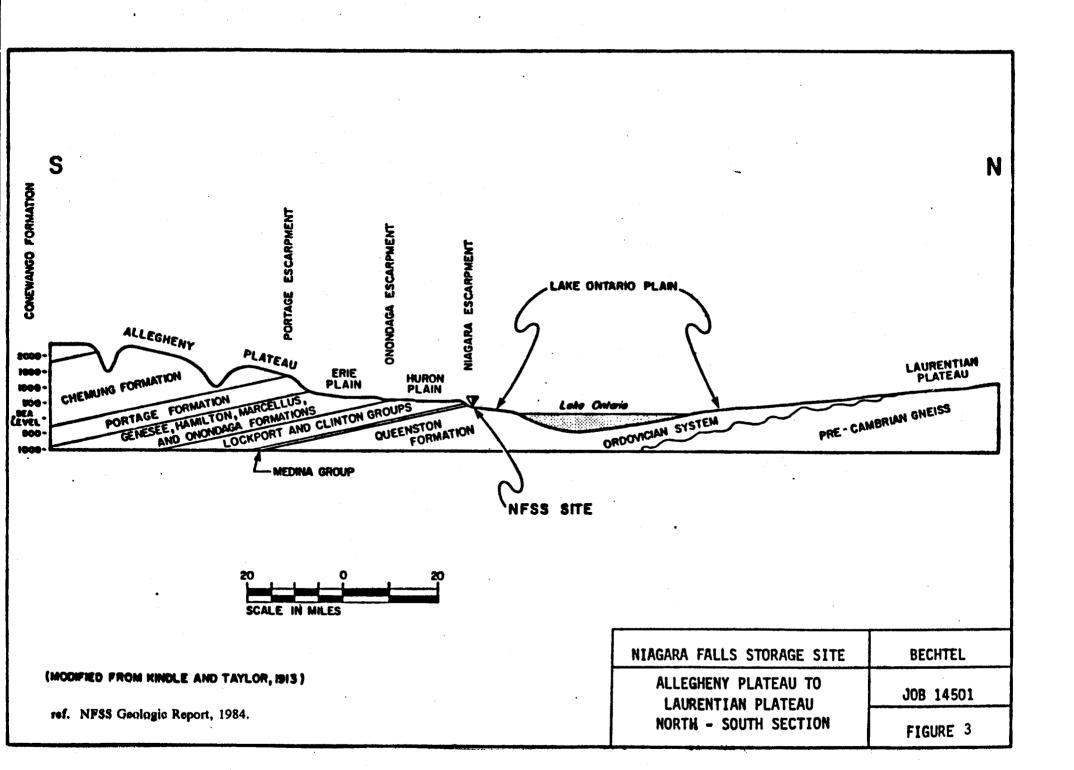
Clinton and Medina Groups

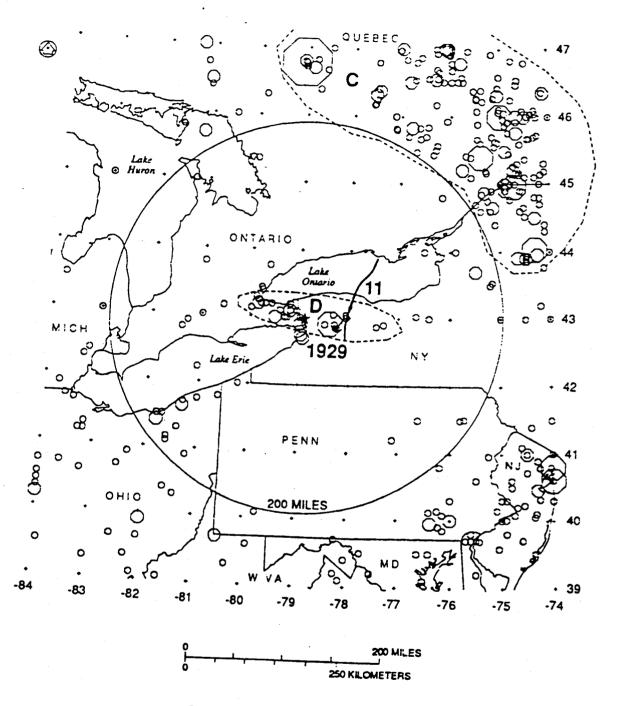
ORDOVICIAN



Queenston Shale







EXPLANATION

Magnitude Scale 3.0-3.9 4.0-4.9 5.0-5.9 6.0-6.9 0

Earthquake locations and magnitude values are from Armbruster and Seeber (1992).

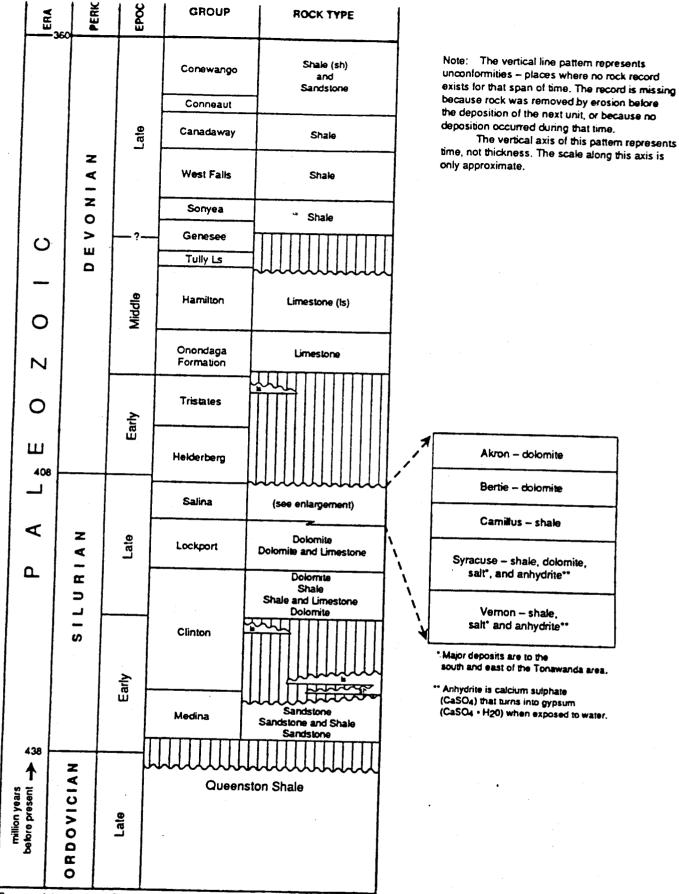
Seismic Source Zones (enclosed by dashed lines)
C = Western Quebec

D = Niagara

11 = Clarendon-Linden structure (bold line)

Data on seismic source zones C and D and structure 11 are from BNI (1986).

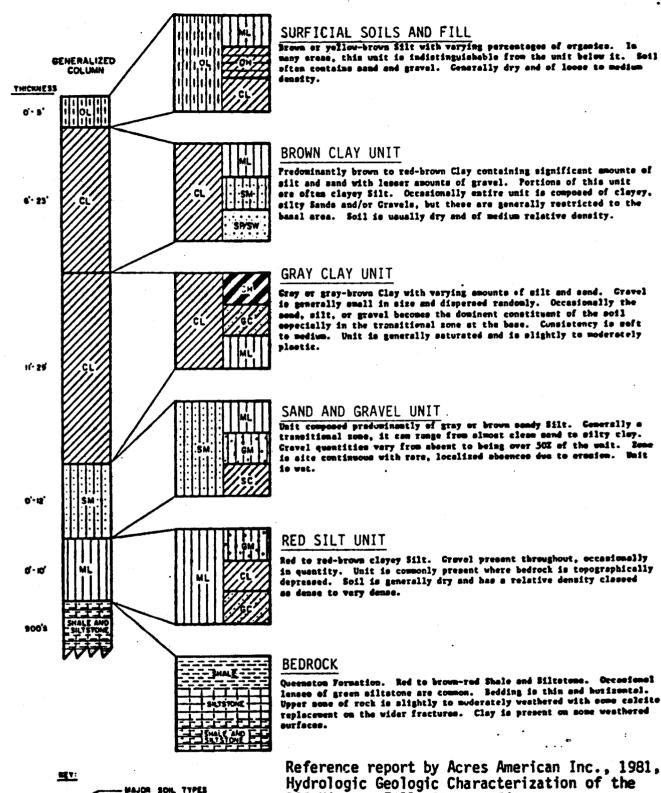
1929 - Location of Attica, New York, earthquake of August 12, 1929 * = Tonawanda Site



Source: Adapted from Rogers et al. 1990.

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DESCRIPTION



SOIL TYPE VARIATIONS OR TRANSITIONAL SOILS

SOR CLASSFICATION BASED ON THE UNIFIED SON, CLASSFICATION BYSTEID" PIGNAE B.S.

ref. NFSS Geologic Report, 1984.

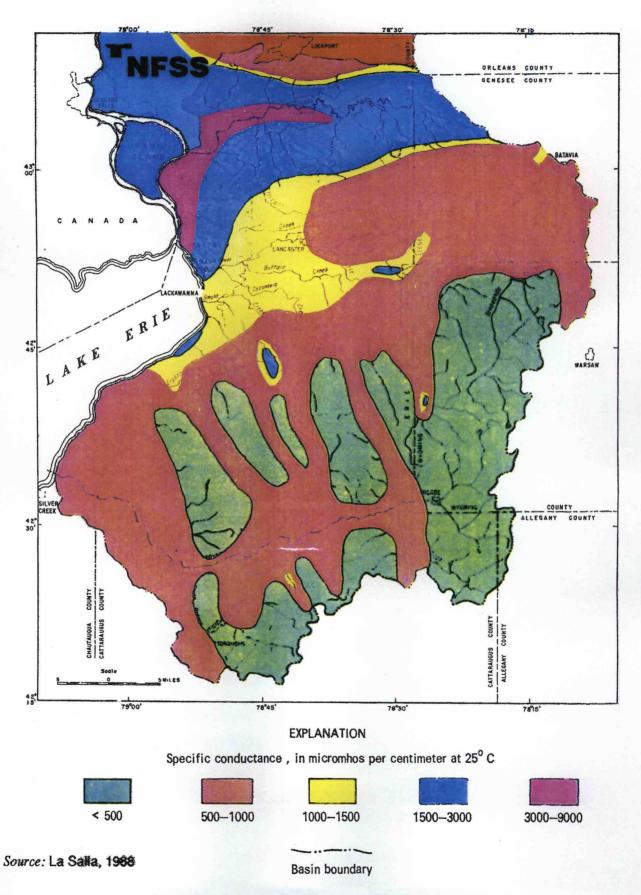
Reference report by Acres American Inc., 1981, DOE-Niagara Falls Storage Site.

| NIAGARA FALLS STORAGE SITE | BECHTEL. | | |
|----------------------------|-----------|--|--|
| GENERALIZED GEOLOGIC | JOB 14501 | | |
| COLUMN | FIGURE 4 | | |

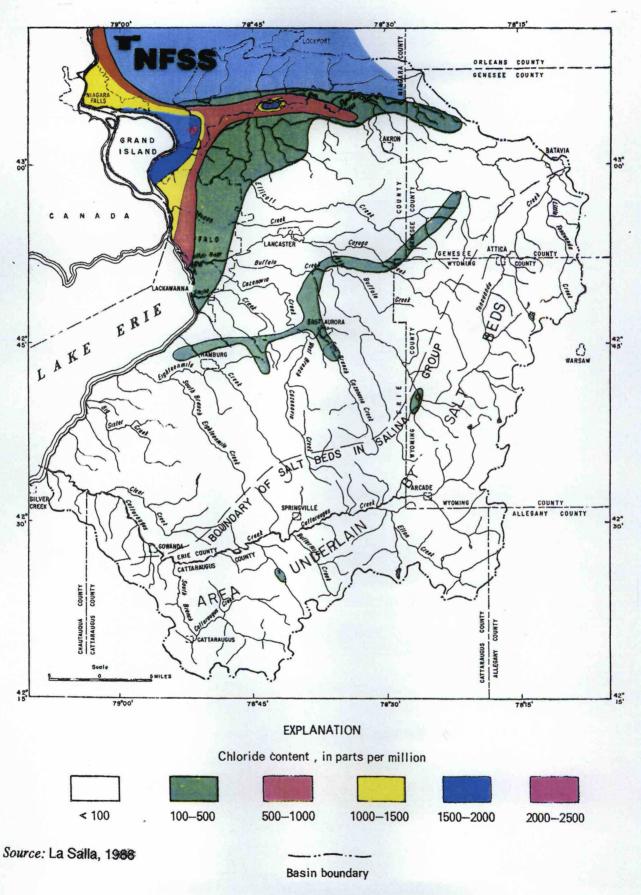
REGIONAL GROUNDWATER ANALYSIS

Water quality data

• Well canvas



Specific Conductance of Water in Bedrock



Chloride Content of Water in Bedrock

TABLE 4

GROUND-WATER QUALITY IN THE CONFINED ALLUVIAL AQUIFER AND FRACTURED SHALE/GLACIAL TILL WATER-BEARING ZONE ON AUGUST 24, 1977

SAMPLING LOCATION

| PARAMETER | | | | | | | | |
|----------------------|--------|--------|--------|--------|--------|-------------------|--------|--------|
| | B-21 | B-22 | B-32 | B-33 | B-34 | B-35 _. | B-36 | B-37 |
| Formation | GT/FS | GT | GT | FS | AL | GT/FS | AL | AL |
| Hq . | 8.6 | 8.6 | 8.2 | 7.7 | 8.3 | 7.8 | 8.1 | 8.3 |
| Sp. Gr. | ,1.002 | 1.004 | 1.002 | 1.005 | 1.022 | 1.003 | 1.003 | 1.005 |
| Conductivity | 730 | 3,350 | 840 | 4,400 | 850 | 1,900 | 370 | 710 |
| (mhos) TC (mg/l) | 18 | 29 | 59 | 36 | 37 | 34 | 73 | 37 |
| TIC (mg/l) | 10 | 5 | 45 | 11 | 27 | 17 | 47 | 17 |
| TOC (mg/1) | 8 | 22 | 14 | 25 | 10 | 17 | 26 | 20 |
| T.D.S. (mg/1) | 552 | 2,842 | 818 | 4,920 | 882 | 1,820 | 376 | 540 |
| COD (mg/l) | 95.2 | 161.6 | 120 | 169.8 | <40 | 89.9 | 140.8 | 171.8 |
| Chloride (mg/l) | 135 | 1,586 | 236 | 1,231 | 287 | 186 | 34 | 160 |
| B (mg/l) | 0.40 | 0.82 | 0.57 | 1.07 | 0.38 | 1.46 | 0.13 | 0.29 |
| Cd (mg/1) | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 |
| Co (mg/1) | <0.01 | <0.01 | 0.02 | 0.03 | 0.01 | 0.03 | 0.02 | <0.01 |
| Cr (mg/l) | <0.01 | 0.03 | 0.01 | <0.01 | <0.01 | 0.01 | 0.03 | 0.01 |
| Cu (mg/l) | 0.44 | 0.70 | 0.63 | 1.2 | <0.01 | 0.30 | 1.2 | 0.58 |
| Fe (mg/l) | 0.18 | 0.37 | 0.36 | 0.98 | 7.4 | 1.0 | 3.4 | 15.4 |
| Ni (mg/l) | 0.08 | 0.06 | <0.01 | 0.14 | 0.07 | <0.01 | 0.04 | 0.14 |
| Mn (mg/l) | 0.14 | 0.28 | 0.40 | 3.0 | 11.0 | 0.74 | 0.75 | 5.2 |
| Zn (mg/l) | 1.2 | 0.31 | 2.2 | 3.5 | 2.8 | 0.46 | 0.52 | 0.72 |
| Se (mg/1) | 0.009 | <0.005 | <0.005 | <0.005 | 0.005 | <0.005 | <0.005 | 0.005 |
| As (mg/l) | 0.003 | 0.004 | 0.003 | <0.003 | <0.003 | 0.003 | 0.005 | <0.003 |
| Hg (mg/l) | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Sulfate (mg/l) | _ | - | - | _ | - | 1,025 | - | - |

FORMATIONS

FS = Fractured Queenston Shale (only)

GT = Pre-Wisconsin Glacial Till

GT/FS = Combined Fractured Shale/

Pre-Wisconsin Glacial Till

AL = Alluvial Aquifer

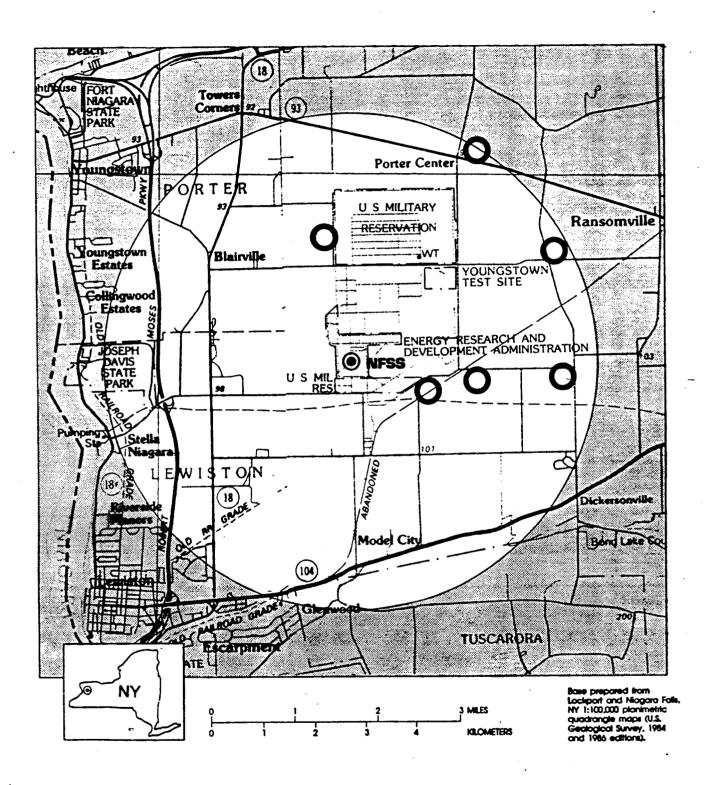
TABLE 4 (Cont'd)

SAMPLING LOCATION

| PARAMETER | B-38 | B-39 | B-40 | B-41 | B-42 | B-43 | B-44 | ъ-45 |
|----------------------|------------|--------|--------|--------|--------|--------|--------|--------|
| Formations | ΑĽ | AL | AL | GT/FS | GT/FS | AL . | AL | GT/FS |
| рН | 8.0 | 7.7 | 8.0 | 8.0 | 8.3 | 7.8 | 8.0 | 7.8 |
| Sp. Gr. | 1.002 | 1.004 | 1.001 | 1.003 | 1.003 | 1.002 | 1.002 | 1.003 |
| Conductivity | 490 | 2,000 | 910 | 1,280 | 1,140 | 1,650 | 1,450 | 2,300 |
| (mhos) TC (mg/1) | 9 9 | 37 | 176 | 58 | 45 | 56 | 26 | 27 |
| TIC (mg/l) | 30 | 11 | 28 | 20 | 13 | 34 | 26 | 11 |
| TOC (mg/1) | 69 | 26 | 148 | 38 | 32 | 22 | 0 | 16 |
| T.D.S. (mg/1) | 420 | 2,662 | 692 | 694 | 2,564 | 1,550 | 1,264 | 2,274 |
| COD (mg/l) | 225.7 | 95.2 | 426.5 | 153.2 | 120.1 | 113.9 | 47.6 | 85.7 |
| Chloride (mg/l) | 93 | 186 | 211 | 262 | 149 | 270 | 230 | 358 |
| B (mg/l) | 0.25 | 0.93 | 0.30 | 0.67 | 0.66 | 0.57 | 0.90 | 0.75 |
| Cd (mg/l) | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 |
| Co (mg/1) | 0.01 | <0.01 | 0.01 | <0.01 | 0.03 | 0.01 | 0.02 | <0.01 |
| Cr (mg/l) | <0.01 | 0.01 | <0.01 | <0.01 | 0.02 | <0.01 | <0.01 | 0.01 |
| Cu (mg/1) | 0.12 | 0.14 | 0.27 | 0.23 | 0.08 | 0.19 | 0.10 | 0.72 |
| Fe (mg/1) | 0.14 | 0.28 | 0.35 | 0.21 | 0.34 | 0.60 | 0.64 | 0.57 |
| Ni (mg/l) | 0.15 | 0.04 | 0.06 | 0.07 | 0.06 | 0.08 | 0.02 | <0.01 |
| Mn (mg/l) | 0.13 | 0.43 | 0.21 | 0.45 | 0.20 | 0.25 | 0.25 | 1.8 |
| Zn (mg/l) | 0.08 | 1.9 | 0.31 | 0.99 | 2.7 | 0.24 | 0.95 | 2.1 |
| Se (mg/l) | <0.005 | <0.005 | <0.005 | <0.005 | <0.005 | 0.005 | <0.005 | <0.005 |
| As (mg/l) | <0.003 | 0.003 | <0.003 | <0.003 | <0.003 | 0.003 | <0.003 | <0.003 |
| Hg (mg/l) | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Sulfate (mg/l) | - | 1,060 | - | 625 | 625 | 475 | 650 | 1,000 |

TABLE 4 (Cont'd)

| | SAMPLING LOCATION | | | | | | | |
|---------------------------|-------------------|--------|--------|--------|--------|--------|--------|--------------------------------|
| PARAMETER | B-46 | B-48 | B-49 | WELL 1 | WELL 2 | WELL 3 | WELL 5 | Drinking Water Standavds |
| Formations | AL | GT/FS | GT/FS | | | • | | # |
| рН | 7.7 | 7.9 | 8.4 | 7.4 | 6.8 | 7.0 | 7.7 | |
| Sp. Gr. | 1.004 | 1.003 | 1.002 | 1.003 | 1.003 | 1.003 | 1.002 | |
| Conductivity | 3,100 | 1,850 | 650 | 2,000 | 1,220 | 1,110 | 710 | |
| (mhos) TC (mg/l) | 42 | 27 | 22 | 11 | 9 | 11 | 58 | |
| TIC (mg/l) | 32 | 12 | 10 | 5 | 0 | 8 | 25 | |
| TOC (mg/1) | 10 | 15 | 12 | 6 | 9 | 3 | 33 | |
| T.D.S. (mg/l) | 3,546 | 1,614 | 518 | 2,082 | 1,276 | 1,104 | 620 | 500 × |
| COD (mg/1) | 89.0 | 82.8 | 51.8 | 43.5 | 40 | 53.8 | 70.4 | |
| <pre>aloride (mg/l)</pre> | 331 | 438 | 81 | 216 | 196 | 230 | 176 | 250 🛊 |
| B (mg/1) | 1.66 | 0.97 | 0.52 | 0.67 | 0.92 | 0.80 | 0.30 | |
| Cd (mg/1) | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | |
| Co (mg/1) | <0.01 | 0.02 | 0.02 | 0.04 | <0.01 | <0.01 | 0.02 | |
| Cr (mg/l) | <0.01 | 0.02 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | |
| Cu (mg/l) | 0.44 | 0.34 | 0.19 | 0.05 | 0.02 | 0.01 | 0.07 | |
| Fe (mg/l) | 1.8 | 0.36 | 1.1 | 9.4 | 20.8 | 5.6 | 0.23 | |
| Ni (mg/l) | 0.05 | <0.01 | <0.01 | <0.01 | 0.06 | 0.03 | 0.05 | |
| Mn (mg/l) . | 0.70 | 1.9 | 0.29 | 0.66 | 0.93 | 0.39 | 0.14 | |
| Zn (mg/l) | 2.8 | 0.13 | 0.60 | 0.10 | 0.06 | 0.04 | 0.28 | |
| Se (mg/1) | <0.005 | <0.005 | <0.005 | <0.005 | <0.005 | <0.005 | 0.005 | |
| As (mg/1) | 0.003 | <0.003 | 0.003 | <0.003 | <0.003 | <0.003 | 0.003 | |
| Hg (mg/l) | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 | |
| Sulfate (mg/l) | 1,000 | 800 | •- | 600 | 1,200 | 620 | - | |

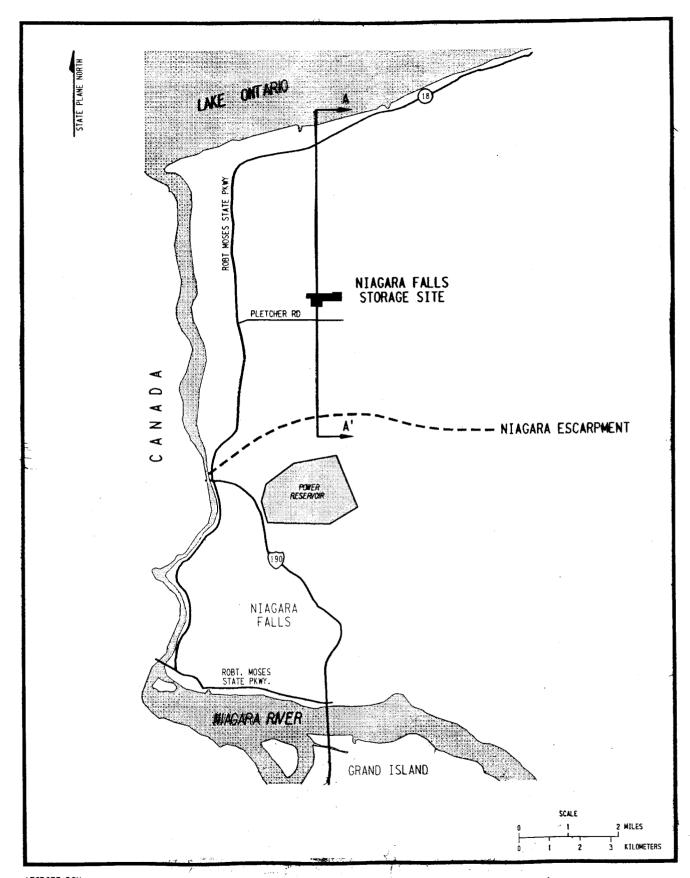


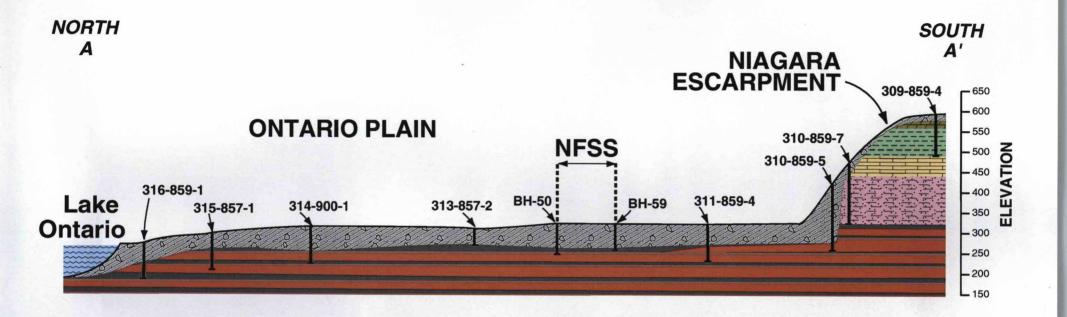
ref. Unpublished Well Canvass Update 1994.

SITE-SPECIFIC GEOLOGY

• Relation to the Niagara escarpment

Stratigraphy





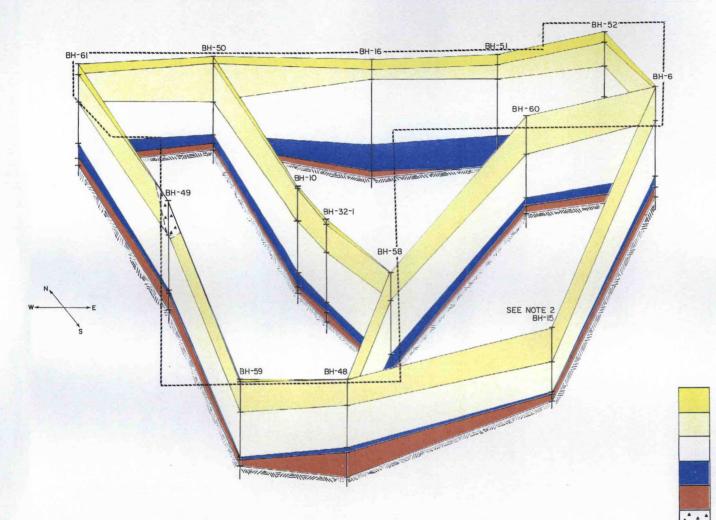
313-857-2 Water well from: Johnson, "Ground Water in the Niagara Falls Area, New York," New York Conservation Dept., Water Resource Commission, Bulletin GW-53, 1964 BH-50 Observation well from: Acres American, Inc., "Hydrologic and Geologic Characterization of the DOE - Storage Site Niagara Falls," prepared Unconsolidated Lacustrine, Alluvial & Glacial Deposits Lockport Dolomite Rochester Shale Clinton Group Albion Sandstones and Shales

Queenston Shale

Source: NFSS analysis of contaminant migration Phase 1 Report, 1982.

for NLO, Inc., Fernald, Ohio, Sept. 30, 1981

EXPLANATION



LEGEND

BROWN SILT WITH ORGANICS. GENERALLY DRY AND OF LOOSE TO MEDIUM DENSITY.

BROWN CLAY CONTAINS VARYING AMOUNTS OF SILT, SAND AND GRAVEL. OFTEN COARSE GRAINED NEAR BASE OF UNIT.

GRAY CLAY, SILTY, SANDY, WITH SOME GRAVEL SOFT TO MEDIUM-SLIGHTLY TO MODERATELY PLASTIC.

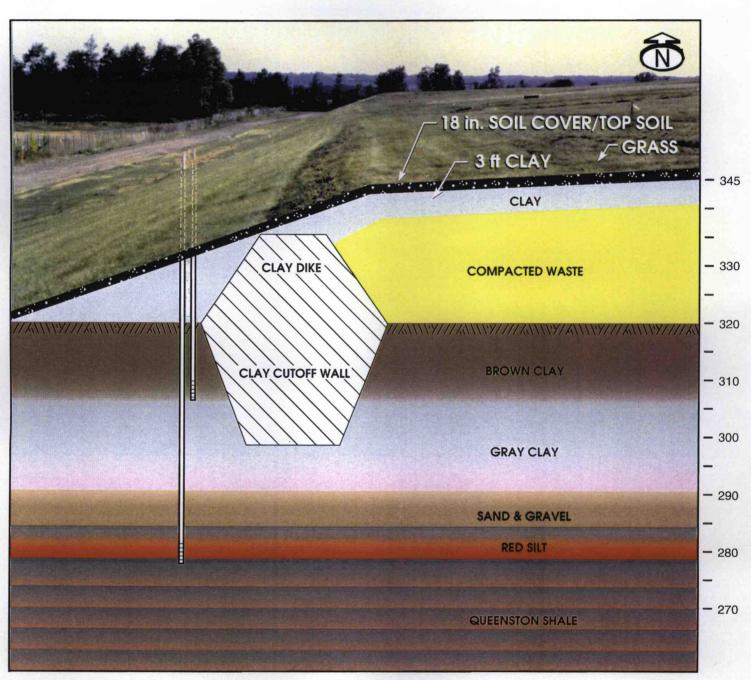
GRAY OR BROWN, SAND OR SILT, GRAVELY WITH SOME CLAY. FINE CONTENT VARIES. UNIT IS WET.

RED CLAYEY SILT, GRAVEL DISPERSED THROUGHOUT. DENSE TO VERY DENSE.

FILL

QUEENSTON FORMATION NFSS SITE BOUNDARY

Source: Acres American, NFSS Geologic Report, 1981.



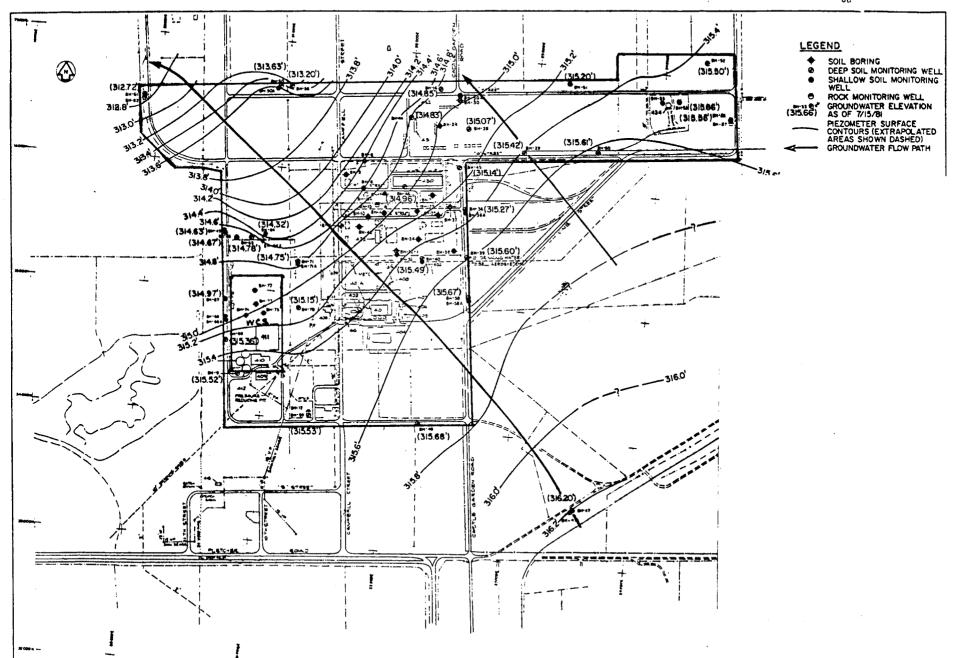
Note: Per Generalized Soil Column NFSS Geologic Report, 1984.

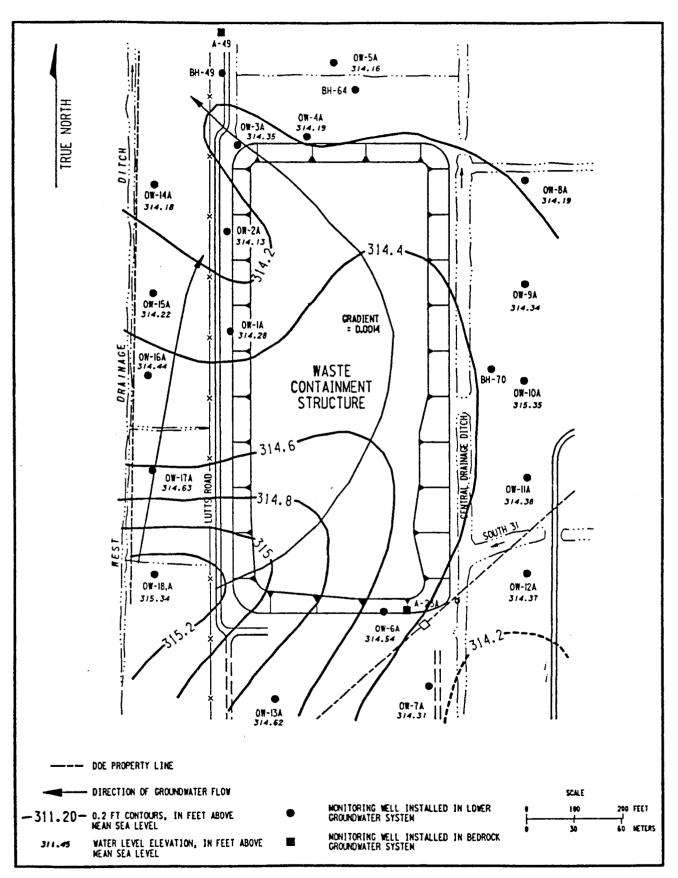
SITE-SPECIFIC HYDROGEOLOGY

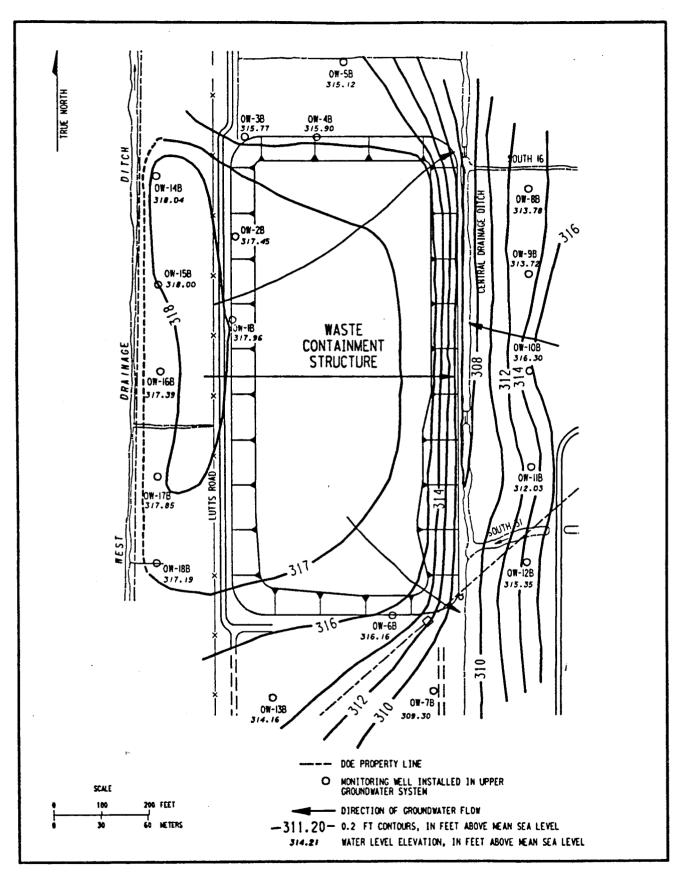
Bedrock gradient

PRECONSTRUCTION/POST—CONSTRUCTION OF THE INTERIM STORAGE CELL

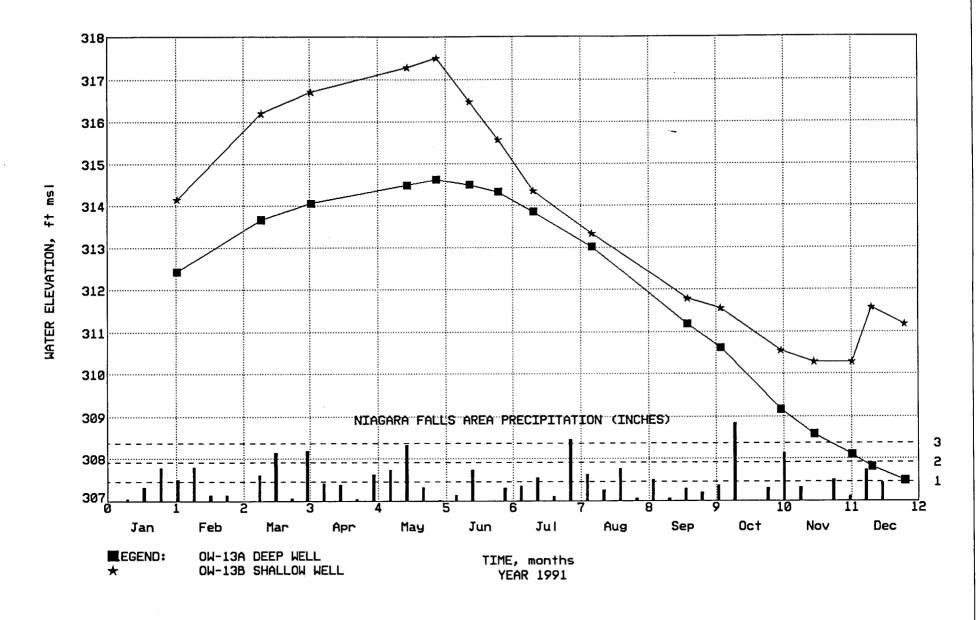
- Water table gradient
- Influence from modern landfill pumping operations



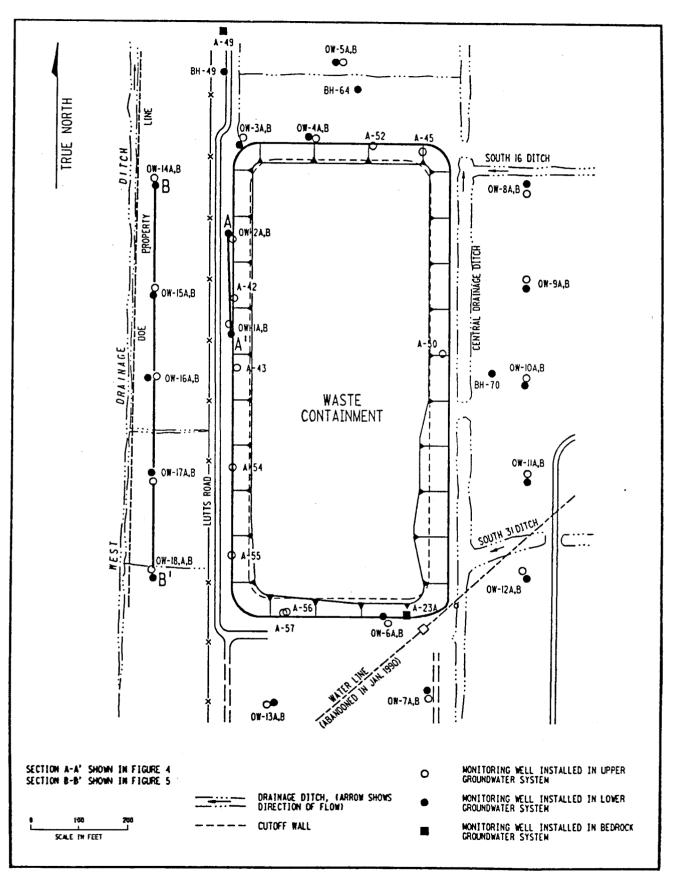


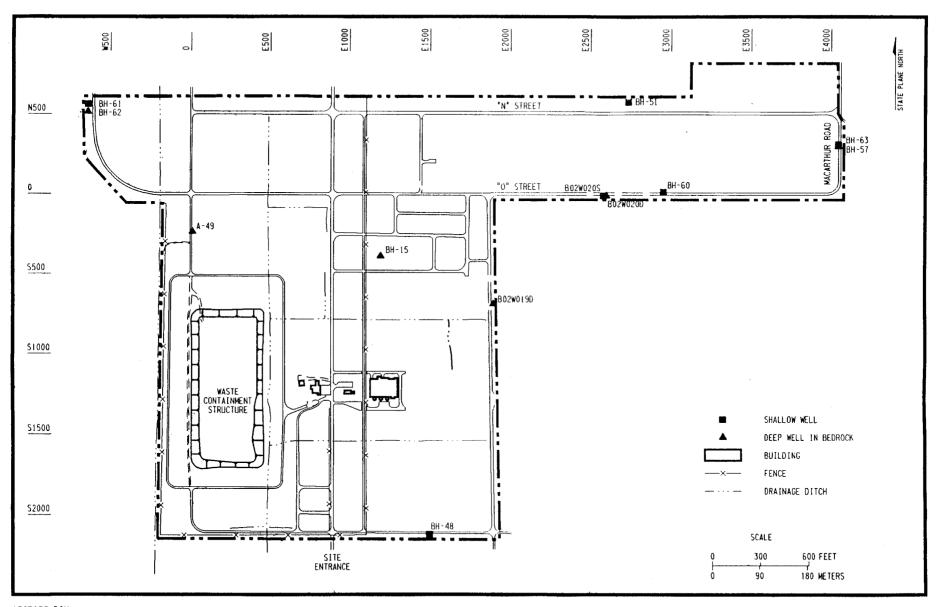


158 R10F007.DGN



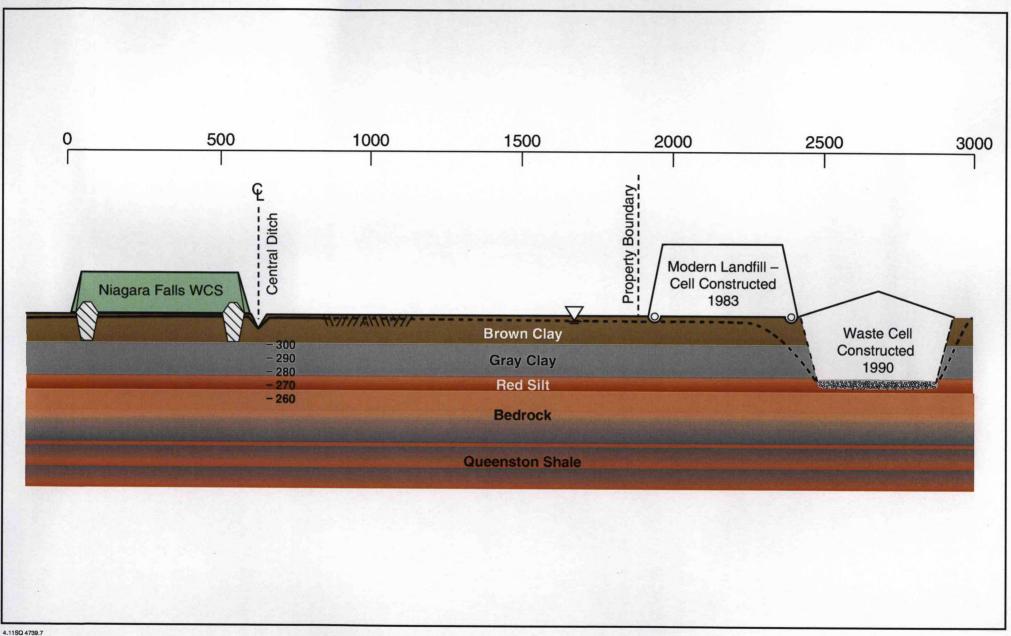
NFSS HYDROGRAPHS

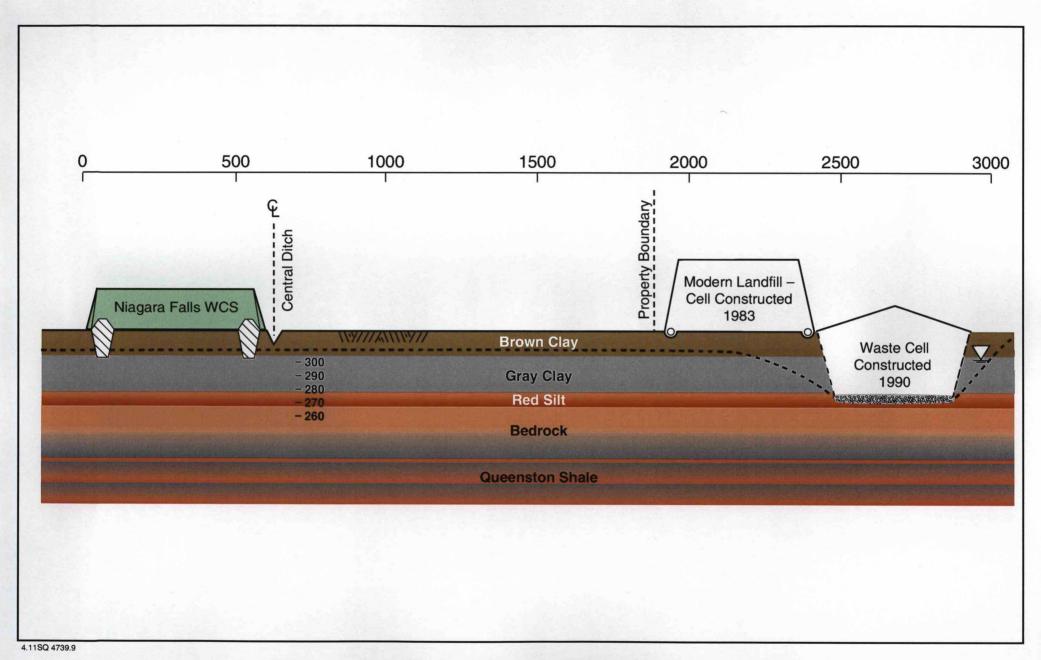


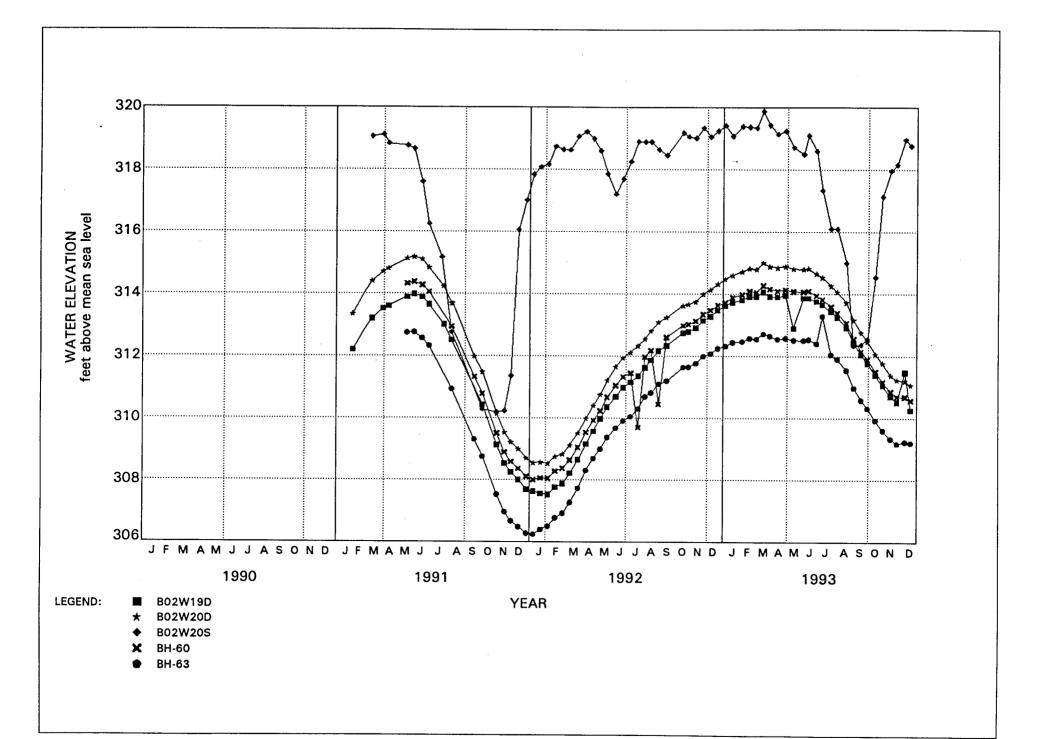


158F 035. DGN

Monitoring Well Locations at the Niagara Falls Storage Site







FACILITY DESIGN

- Design criteria
- Interim cap design
- Final cap design
- Cutoff wall construction
- Monitoring systems and procedures
 - Monitoring wells outside the cutoff wall
 - VWPTs inside the pile
 - Annual walkover and inspection

DESIGN REQUIREMENTS FOR THE NESS WASTE CONTAINMENT FACILITY

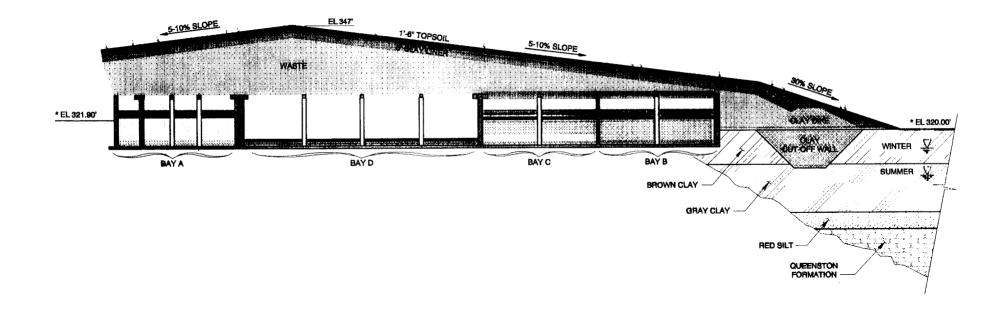
Page 1 of 2

| Item No. | Description | Existing Cap | Long-Term Cap | Dike and Cutoff Walls | Bottom | Remarks | |
|-------------|---|--------------------------------|--|-------------------------------|-------------------------------|--------------------|--|
| 1. | Design Service Life | 25-50 years | 200-1000 years | 200-1000 years | 200-1000 years | | |
| 2. | Safety Factor: Cutoff Walls Slope Stability Static conditions Earthquake | 1.5 | 1.5 1.0 | | | | |
| 3. | Surface Drainage Slope Top Surface Side Slopes | 5-10 \$ Max. 3H to IV | 5-10 \$ Max. 5H to 1V | | , | | |
| 4. | Surface Erosion Protection | Shallow-rooted grass | Shallow-rooted grass Riprap to elevation 98.4 m (323 ft) | | | | |
| 5. | Intrusion Barrier Required | No | Yes | | | | |
| 6. | Frost Penetration | 48 in. | 48 In. | | - | Assume bare ground | |
| 7. | Radon Barrier Required | Yes (20 pC1/m ² /s) | Yes (20 pC1/m ² /s) | · | | ground | |
| 8. | Radiation Barrier Required | Yes (100 mrem/yr) | Yes (100 mrem/yr) | | | | |
| 9. | Component Construction | Topsoll/clay | Topsoll/rock layer/clay | Clay | Natural clay strata | | |
| 10. | Clay Permeability | 10 ⁻⁷ cm/s | 10 ⁻⁷ cm/s | Λρρτοχ. 10 ⁻⁷ cm/s | Approx. 10 ⁻⁷ cm/s | | |
| 11. | Clay Adsorption Coefficient Natural Uranium Radium-226 | 5 ml/g 500 ml/g | 5 ml/g 500 ml/g | 5 ml/g 500 ml/g | 5 ml/g 500 ml/g | | |
| 12. | Inspection and Maintenance Required | Yes (design life) | Yes | No | No | | |
| 13. | Earthquake Pseudostatic Coefficient | 0.1g | 0.15g | 0.15 g | | | |

| No. 1 | Description | Existing Interim Cap | Long-Term Cap | Dike and Cutoff Walls | Bottom | | |
|-------|--|--|--|--|--|--|--|
| 14. | DOE Concentration Guide for Radionucilde Migration (groundwater concentration, uncontrolled areas) Natural Uranium Radium-226, -228 | | | 600 pCI/I | 600 pC1/I | | |
| | · | | | 30 pCI/I | 30 pCI/I | | |
| 15. | Temperature Extremes | -29° to 34°C (-20° to 94°F) | -29° to 34°C (-20° to 94°F) | -29° to 34°C (-20° to 94°F) | · — | | |
| 16. | Rainfall per Year | 74 cm (29 ln.) | 74 cm (29 fn.) | •- | | | |
| 17. | Wind Speed and Direction | (80 mph) southwest | (80 mph) southwest | | | | |
| 18. | Annual Deep-Inflitration Rate | 2.54 cm (1.0 ln.) | 2.54 cm (1.0 ln.) | | | | |
| 19. | Design Flood Plain Elevation | Elevation 96.6 m (317 ft) m.s.l. per 100 years | Probable Maximum Flood (PMF) 98.4 m (323 ft) | Probable Maximum Flood (PMF) 98.4 m (323 ft) | | | |
| 20. | Groundwater Elevation (high) | | | | Elevation 96 m (315 ft) m.s.l. (Exclusive of PMF) | | |
| 21. | Snowfall Per Year | 2.4 m (93 ln.) | 2.4 m (93 ln.) | | | | |
| 22. | Internal Cap Drainage Layer | None | Yes | | **** | | |
| 23. | Waste Containment Consolidation | Minimize settlement (95% compaction) | Minimize settlement (95% compaction) | 95% compaction | | | |
| 24. | Shrinkage, Swelling, and Frost Action Requirements | Yes (3 to 5% in volume expansion) | Yes (3 to 5% in volume expansion) | Yes (3 to 5≴ In volume expansion) | No | | |
| 25. | Migration Limits * | Not to exceed EPA primary drinking water standards in off-site groundwater | Not to exceed EPA primary drinking water standards in off-site groundwater | Not to exceed EPA primary drinking water standards in off-site groundwater | Not to exceed EPA primary drinking water standards in off-site groundwater | | |
| 26. | Buffer Zone (measured from lateral limit of waste) | 30.5 m (100 ft) | 30.5 m (100 ft) | | | | |
| 27. | Groundwater Hydraulic Gradient (saturated zone) | | | | 0.0015 | | |

Remarks

NIAGARA FALLS STORAGE SITE **CROSS SECTION OF INTERIM WASTE CONTAINMENT STRUCTURE AND BUILDING 411**



CONTAMINATED SOIL FILL

INITIAL UNCOMPACTED SOIL FILL



COMPACTED CLAY COVER



EXISTING SAND FILTER

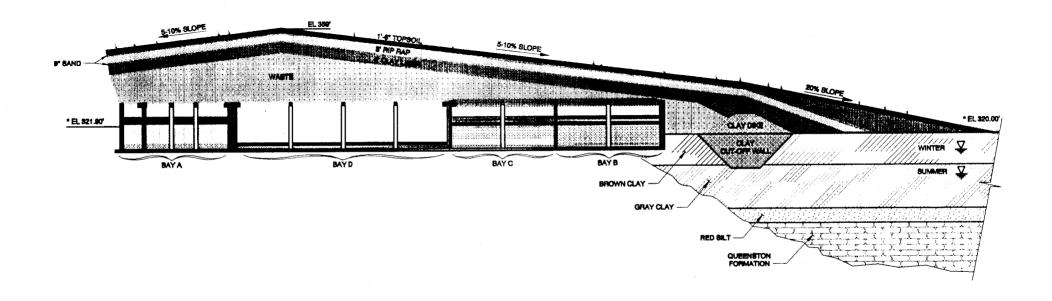
SAND LAYER

EXISTING L-30 AND F-32 RESIDUES

EXISTING K-65 RESIDUES

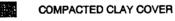
GEOTEXTILE FABRIC

NIAGARA FALLS STORAGE SITE CROSS SECTION OF FINAL WASTE CONTAINMENT STRUCTURE AND BUILDING 411



CONTAMINATED SOIL FILL

INITIAL UNCOMPACTED SOIL FILL



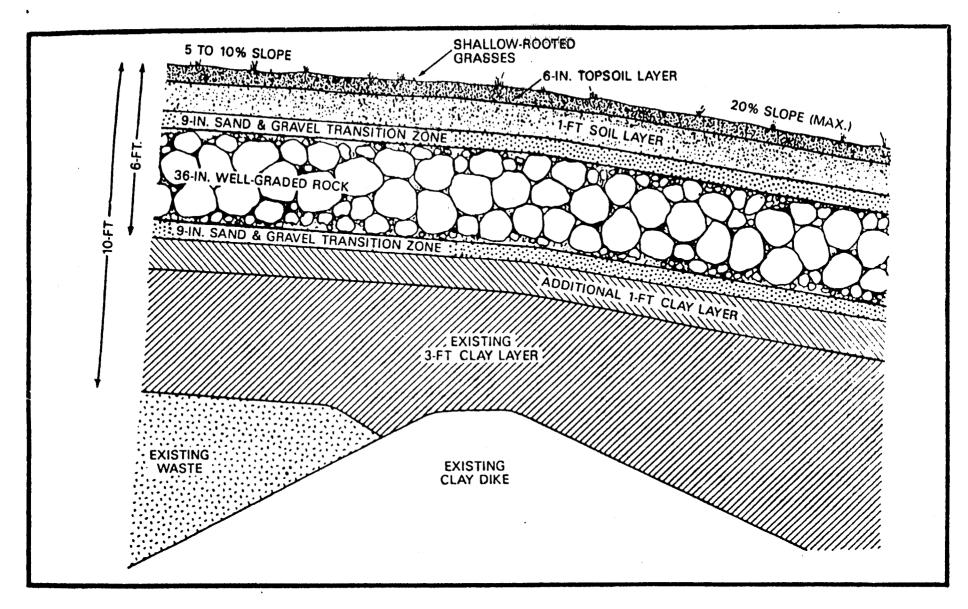
EXISTING SAND FILTER

SAND LAYER

EXISTING L-30 AND F-32 RESIDUES

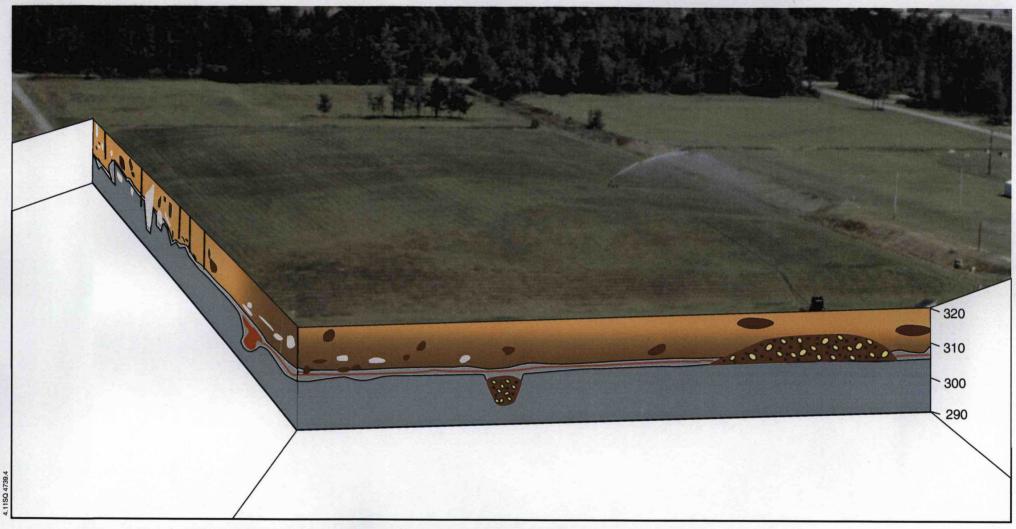
EXISTING K-65 RESIDUES

GEOTEXTILE FABRIC

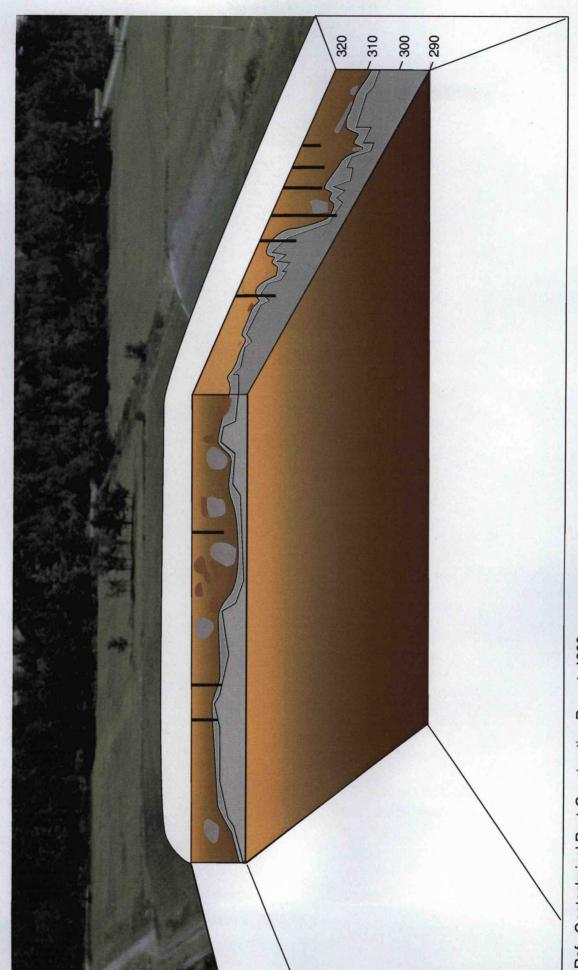


NFSS LONG-TERM COVER LAYERS



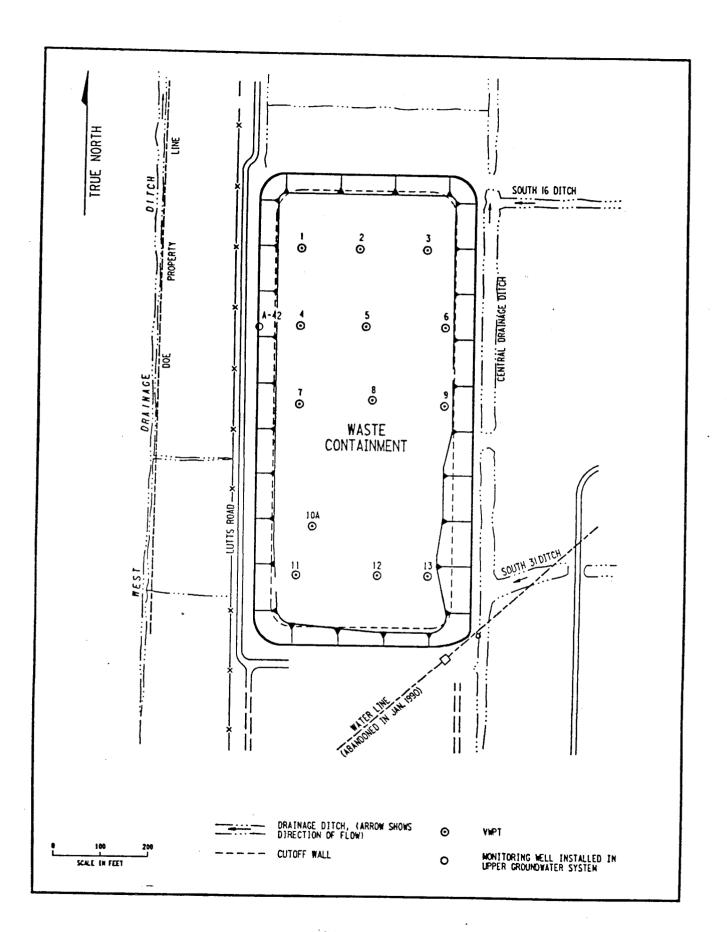


Ref. Geotechnical Post-Construction Report, 1986 NFSS Geologic Report, 1984



Ref. Geotechnical Post-Construction Report, 1986 NFSS Geologic Report, 1984

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VWPT LOCATIONS

VERIFICATION OF GEOTECHNICAL INPUT PARAMETERS FROM NFSS EIS

VERIFICATION

EIS PARAMETERS

| 0.00008 m/yr | 1.8 g/cc | 1.7 g/cc | 10 gal/min | 0.1 | 0.4 | 0.85 | 0.14 m/yr | 0.0016 | 0.89 m/yr | 0.14 m/yr | ı | 0.2 | ı | 16 | ı | 16 | 200 | 100 | 000'9 | 0.107 | 0.2 |
|--------------|------------|------------|-----------------|--------------------|----------|----------------|--------------|-----------------|---------------|---------------|---------------|---------------------------|-----------|-------|-------|-------|--------|--------|--------|--------------|--------|
| 0.0 m/yr | 1.8 g/cc | 1.7 g/cc | 4 or 10 gal/min | 0.1 | 0.4 | 0.85 | 0.14 m/yr | 0.0016 or 0.001 | 0.89 m/yr | 0.14 m/yr | ш 6 | 0.2 | 2 | 16 | 16 | 16 | | 1 | ı | 0.107 | 0.2 |
| Erosion rate | Density c2 | Density s2 | Well intake | Effective porosity | Porosity | ET coefficient | K saturation | Gradient | Precipitation | K unsaturated | T unsaturated | Effective Porosity | Kd Cs-137 | U-234 | U-236 | U-238 | Ra-226 | Pb-210 | Th-230 | Infiltration | Runoff |

Both models assume no dispersion or diffusion